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PORT STANVAC – SOUTH AUSTRALIA

LAT 35° 7' S LONG 138° 28' E

2023

Times and Heights of High and Low Waters

Local Time

| MAY | | | | JUNE | | | | JULY | | | | AUGUST | | | |
|-----------------------------------------------------------------|---|-----------------------------------------------------------------|---|-----------------------------------------------------------------|---|-----------------------------------------------------------------|---|-----------------------------------------------------------------|---|-----------------------------------------------------------------|---|----------------------------------------------------------------|---|-----------------------------------------------------------------|---|
| Time | m | Time | m | Time | m | Time | m | Time | m | Time | m | Time | m | Time | m |
| 1 0211 1.44 0900 0.74 MO 1538 1.61 2123 0.91 | | 16 0246 1.51 0848 0.73 TU 1517 1.80 2134 0.68 | | 1 0253 1.60 0834 0.73 TH 1502 2.11 2140 0.53 | | 16 0326 1.38 0824 0.85 FR 1507 2.22 2211 0.49 | | 1 0328 1.41 0817 0.97 SA 1500 2.21 2213 0.45 | | 16 0425 1.33 0855 0.98 SU 1540 2.19 2252 0.47 | | 1 0539 1.46 1011 0.96 TU 1636 2.34 2345 0.23 | | 16 0520 1.63 1039 0.69 WE 1654 2.26 ● 2333 0.31 | |
| 2 0309 1.66 0923 0.58 TU 1545 1.84 2147 0.65 | | 17 0328 1.61 0911 0.66 WE 1532 2.02 2202 0.48 | | 2 0338 1.65 0906 0.71 FR 1529 2.27 2214 0.38 | | 17 0403 1.43 0902 0.81 SA 1540 2.33 2242 0.42 | | 2 0425 1.45 0907 0.95 SU 1543 2.35 2256 0.34 | | 17 0453 1.45 0946 0.89 MO 1618 2.29 2320 0.40 | | 2 0558 1.48 1045 0.82 WE 1709 2.40 ○ | | 17 0531 1.69 1059 0.59 TH 1713 2.28 2347 0.31 | |
| 3 0343 1.79 0943 0.50 WE 1558 2.01 2211 0.47 | | 18 0357 1.63 0928 0.64 TH 1547 2.19 2226 0.38 | | 3 0414 1.64 0932 0.71 SA 1555 2.40 2248 0.31 | | 18 0432 1.47 0935 0.77 SU 1611 2.41 ● 2311 0.39 | | 3 0506 1.46 0947 0.91 MO 1621 2.44 ○ 2335 0.30 | | 18 0515 1.54 1023 0.79 TU 1649 2.36 ● 2343 0.38 | | 3 0009 0.25 0611 1.51 TH 1115 0.70 1738 2.37 | | 18 0543 1.75 1121 0.52 FR 1733 2.26 | |
| 4 0409 1.83 0958 0.47 TH 1611 2.16 2233 0.34 | | 19 0418 1.60 0940 0.62 FR 1603 2.32 2249 0.33 | | 4 0447 1.59 0956 0.72 SU 1623 2.49 ○ 2322 0.28 | | 19 0459 1.51 1008 0.73 MO 1642 2.45 2340 0.39 | | 4 0540 1.44 1023 0.86 TU 1658 2.49 | | 19 0536 1.60 1054 0.71 WE 1717 2.38 | | 4 0030 0.31 0624 1.56 FR 1146 0.62 1805 2.27 | | 19 0001 0.31 0559 1.81 SA 1146 0.48 1753 2.20 | |
| 5 0430 1.81 1012 0.48 FR 1625 2.28 2257 0.27 | | 20 0435 1.57 0955 0.59 SA 1623 2.42 ● 2313 0.32 | | 5 0517 1.53 1022 0.72 MO 1655 2.52 | | 20 0527 1.55 1042 0.70 TU 1714 2.45 | | 5 0011 0.31 0609 1.43 WE 1059 0.81 1734 2.47 | | 20 0005 0.37 0558 1.65 TH 1123 0.65 1744 2.37 | | 5 0045 0.38 0639 1.65 SA 1217 0.58 1827 2.12 | | 20 0018 0.31 0620 1.87 SU 1212 0.47 1815 2.11 | |
| 6 0452 1.76 1027 0.48 SA 1644 2.39 ○ 2324 0.23 | | 21 0456 1.55 1016 0.56 SU 1648 2.48 2339 0.34 | | 6 0000 0.31 0549 1.46 TU 1049 0.73 1728 2.50 | | 21 0009 0.41 0557 1.58 WE 1116 0.69 1746 2.42 | | 6 0044 0.36 0635 1.43 TH 1134 0.77 1808 2.38 | | 21 0028 0.38 0622 1.70 FR 1154 0.62 1811 2.32 | | 6 0057 0.43 0657 1.76 SU 1247 0.60 1845 1.95 | | 21 0035 0.32 0643 1.93 MO 1241 0.49 1838 1.99 | |
| 7 0516 1.68 1044 0.50 SU 1708 2.45 2355 0.25 | | 22 0521 1.55 1042 0.55 MO 1717 2.48 | | 7 0037 0.39 0619 1.39 WE 1116 0.75 1800 2.42 | | 22 0038 0.44 0628 1.60 TH 1150 0.70 1817 2.35 | | 7 0112 0.44 0659 1.46 FR 1209 0.76 1838 2.25 | | 22 0050 0.38 0650 1.74 SA 1226 0.63 1838 2.23 | | 7 0104 0.44 0717 1.88 MO 1318 0.64 1902 1.80 | | 22 0051 0.34 0706 1.99 TU 1311 0.52 1859 1.87 | |
| 8 0543 1.57 1103 0.53 MO 1734 2.46 | | 23 0009 0.38 0550 1.54 TU 1110 0.58 1748 2.43 | | 8 0111 0.49 0645 1.34 TH 1143 0.77 1830 2.30 | | 23 0106 0.47 0659 1.61 FR 1224 0.73 1847 2.25 | | 8 0134 0.52 0723 1.52 SA 1245 0.77 1904 2.08 | | 23 0113 0.40 0718 1.78 SU 1259 0.66 1904 2.12 | | 8 0113 0.41 0742 1.98 TU 1350 0.70 ● 1920 1.67 | | 23 0106 0.36 0730 2.04 WE 1342 0.57 1922 1.73 | |
| 9 0027 0.33 0607 1.46 TU 1121 0.57 1800 2.41 | | 24 0038 0.44 0619 1.52 WE 1139 0.62 1817 2.34 | | 9 0141 0.60 0711 1.33 FR 1212 0.81 1859 2.14 | | 24 0135 0.51 0732 1.63 SA 1259 0.78 1918 2.14 | | 9 0149 0.57 0749 1.62 SU 1325 0.81 1930 1.91 | | 24 0135 0.42 0748 1.84 MO 1335 0.70 1932 1.98 | | 9 0127 0.39 0813 2.03 WE 1427 0.81 1941 1.52 | | 24 0123 0.41 0756 2.06 TH 1418 0.66 ● 1944 1.55 | |
| 10 0056 0.44 0626 1.37 WE 1136 0.60 1823 2.33 | | 25 0106 0.51 0647 1.51 TH 1208 0.67 1845 2.24 | | 10 0208 0.69 0743 1.35 SA 1250 0.88 1932 1.95 | | 25 0205 0.55 0813 1.65 SU 1342 0.86 1954 1.98 | | 10 0205 0.59 0824 1.73 MO 1414 0.88 ● 2001 1.72 | | 25 0158 0.45 0821 1.89 TU 1417 0.76 2005 1.82 | | 10 0146 0.44 0849 1.99 TH 1516 0.96 1956 1.34 | | 25 0139 0.51 0828 2.00 FR 1507 0.83 2000 1.30 | |
| 11 0122 0.56 0641 1.30 TH 1151 0.63 1847 2.20 | | 26 0135 0.58 0719 1.49 FR 1239 0.76 1916 2.10 | | 11 0240 0.76 0838 1.39 SU 1348 1.02 ● 2017 1.71 | | 26 0240 0.60 0903 1.67 MO 1439 0.96 ● 2041 1.79 | | 11 0226 0.60 0910 1.80 TU 1517 0.98 2037 1.50 | | 26 0224 0.52 0900 1.91 WE 1509 0.84 ● 2043 1.60 | | 11 0203 0.58 0937 1.84 FR 1724 1.14 1859 1.14 | | 26 0142 0.67 0907 1.84 SA | |
| 12 0149 0.69 0700 1.24 FR 1208 0.72 ● 1913 2.00 | | 27 0209 0.66 0801 1.45 SA 1316 0.89 1953 1.91 | | 12 0328 0.84 1016 1.45 MO 1554 1.17 2138 1.44 | | 27 0325 0.69 1009 1.70 TU 1605 1.05 2150 1.57 | | 12 0255 0.67 1009 1.84 WE 1702 1.07 2128 1.26 | | 27 0253 0.64 0947 1.90 TH 1627 0.95 2133 1.33 | | 12 0143 0.78 1125 1.66 SA 2258 0.79 | | 27 0026 0.78 1047 1.60 SU 2246 0.57 | |
| 13 0230 0.85 0725 1.15 SA 1212 0.89 1941 1.71 | | 28 0300 0.77 0912 1.38 SU 1410 1.09 ● 2051 1.67 | | 13 0453 0.91 1224 1.62 TU 1933 1.06 | | 28 0425 0.80 1129 1.76 WE 1815 1.03 2342 1.39 | | 13 0333 0.80 1134 1.84 TH 2018 0.98 | | 28 0322 0.83 1056 1.85 FR 1924 0.95 | | 13 1507 1.82 2239 0.58 SU | | 28 0600 1.37 0919 1.27 MO 1527 1.87 2252 0.32 | |
| 14 0543 1.00 1802 1.37 SU 2156 1.34 | | 29 0433 0.88 1155 1.42 MO 1727 1.23 2325 1.47 | | 14 0033 1.29 0628 0.92 WE 1340 1.85 2052 0.81 | | 29 0545 0.90 1255 1.89 TH 2012 0.84 | | 14 0002 1.05 0441 0.97 FR 1331 1.91 2139 0.76 | | 29 0031 1.06 0331 1.04 SA 1312 1.85 2150 0.68 | | 14 0504 1.37 0935 1.02 MO 1557 2.03 2257 0.42 | | 29 0528 1.49 1005 1.00 TU 1613 2.12 2313 0.17 | |
| 15 0040 1.36 0820 0.85 MO 1515 1.53 2105 0.98 | | 30 0638 0.87 1342 1.65 TU 2009 1.00 | | 15 0228 1.32 0737 0.89 TH 1430 2.06 2136 0.61 | | 30 0157 1.35 0710 0.96 FR 1406 2.05 2122 0.62 | | 15 0340 1.17 0728 1.05 SA 1450 2.05 2220 0.59 | | 30 0458 1.25 0745 1.19 SU 1458 2.03 2239 0.44 | | 15 0508 1.53 1013 0.83 TU 1629 2.18 2317 0.33 | | 30 0533 1.58 1033 0.77 WE 1646 2.25 2331 0.16 | |
| | | 31 0143 1.51 0751 0.79 WE 1429 1.90 2102 0.73 | | | | | | | | 31 0516 1.39 0923 1.10 MO 1555 2.21 2315 0.28 | | | | 31 0541 1.62 1056 0.60 TH 1710 2.26 ○ 2344 0.22 | |

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Datum of Predictions is Lowest Astronomical Tide

Caution: Predictions are of secondary quality

Times are in local standard time (UTC +09:30) or daylight savings time (UTC +10:30) when in effect

Moon Phase Symbols

● New Moon

◐ First Quarter

○ Full Moon

◑ Last Quarter

